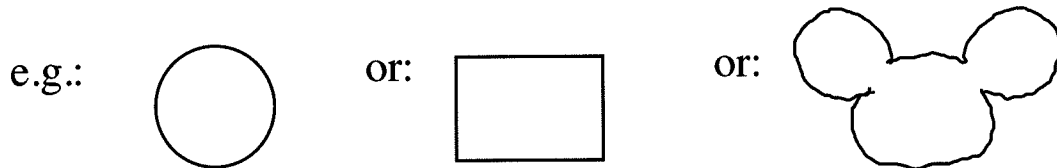


METR 3123, Atmospheric Dynamics II

LECTURE 25

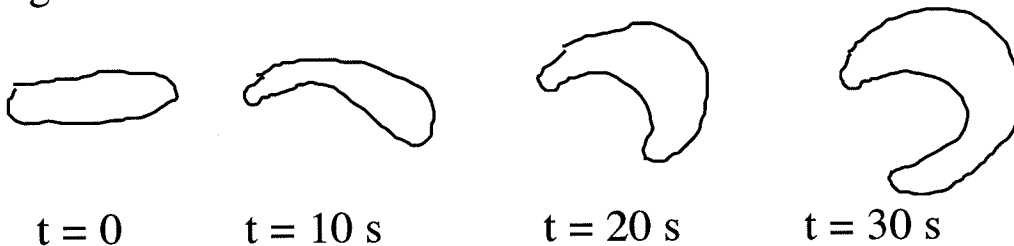
Circulation Theorem

Consider any arbitrary closed curve drawn in the flow:



This curve is composed of fluid. As time goes on, this curve moves with the flow and distorts in shape, but it's always composed of same fluid elements. It's a material curve (curve that's always composed of same fluid elements).

e.g.: a closed material curve at dif times:

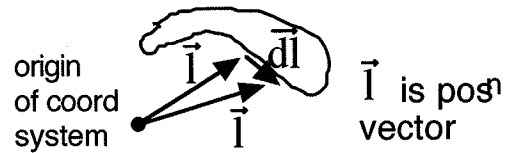


In general, the circulation around the closed material curve is a function of time:

$$C(t) = \oint \vec{u} \cdot d\vec{l}$$

Lets find an expression for rate of change of absolute circulation around a material curve [equivalent to rate of change of area-integrated absolute vorticity via Stokes thm]

$$C_a(t) = \oint \vec{u}_a \cdot \vec{dl}$$



$$\frac{D_a C_a}{Dt} = \frac{D_a}{Dt} \oint \vec{u}_a \cdot \vec{dl}$$

$$= \oint \left[\frac{D_a \vec{u}_a}{Dt} \right] \cdot \vec{dl} + \oint \vec{u}_a \cdot \left[\frac{D_a \vec{dl}}{Dt} \right] \rightarrow d \left(\frac{D_a \vec{l}}{Dt} \right) \rightarrow d\vec{u}_a$$

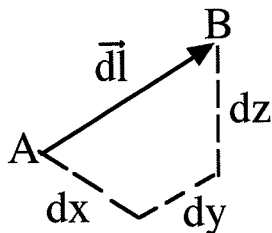
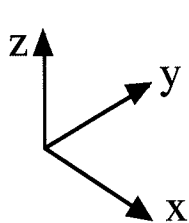
use eqn of motion (neglecting friction):

$$\frac{D_a \vec{u}_a}{Dt} = -\frac{1}{\rho} \nabla p + \vec{g}, \text{ where } \vec{g} = -g\hat{k} = -\nabla(gz) = -\nabla\Phi$$

$$\therefore \frac{D_a C_a}{Dt} = -\oint \frac{1}{\rho} \nabla p \cdot \vec{dl} - \oint \nabla\Phi \cdot \vec{dl} + \oint \vec{u}_a \cdot d\vec{u}_a$$

\downarrow \downarrow
 $\frac{DC_a}{Dt}$ since C_a is a scalar $\frac{1}{2} d(\vec{u}_a \cdot \vec{u}_a)$

Scratch paper: How does p vary across the line element \vec{dl} ?



$$\vec{dl} = dx \hat{i} + dy \hat{j} + dz \hat{k}$$

Use Taylor expansion for p_B about point A.

$$p_B = p_A + \left. \frac{\partial p}{\partial x} \right|_A dx + \left. \frac{\partial p}{\partial y} \right|_A dy + \left. \frac{\partial p}{\partial z} \right|_A dz$$

$$dp = p_B - p_A = \left. \frac{\partial p}{\partial x} \right|_A dx + \left. \frac{\partial p}{\partial y} \right|_A dy + \left. \frac{\partial p}{\partial z} \right|_A dz$$

$$= \nabla p \cdot \vec{dl}$$

So $\nabla p \cdot \vec{dl} = dp$

In general, change in any scalar over a directed distance \vec{dl} is:

$$d(\text{scalar}) = \nabla(\text{scalar}) \cdot \vec{dl}$$

end of scratch paper

$$\therefore \frac{DC_a}{Dt} = - \oint \frac{dp}{\rho} - \underbrace{\oint d\Phi}_{\downarrow} + \frac{1}{2} \underbrace{\oint d(\vec{u}_a \cdot \vec{u}_a)}_{\downarrow}$$

$\Phi_{\text{endpoint}} - \Phi_{\text{startpoint}} = 0$ 0 for same reason
 since end/start points are the same for a closed curve

$$\therefore \boxed{\frac{DC_a}{Dt} = - \oint \frac{dp}{\rho}}$$
 Rate of change of absolute circulation is due only to baroclinic forcing.

Can show that in a barotropic fluid, $\oint \frac{dp}{\rho} = 0$. Then:

$$\boxed{\frac{DC_a}{Dt} = 0} \quad \text{Kelvin's Circulation Theorem.}$$

so $C_a = \text{const}$ for a closed material curve.

Means that: "Absolute circulation is conserved following fluid motion in a frictionless barotropic fluid"

Now lets relate absolute circulation C_a to relative circ C :

$$\begin{aligned} C_a &= \oint \vec{u}_a \cdot d\vec{l} = \oint \left(\vec{u} + \vec{\Omega} \times \vec{r} \right) \cdot d\vec{l} \\ &\quad \downarrow \qquad \qquad \downarrow \\ &\quad \text{rel velocity} \quad \text{pos}^n \text{ vector (same as } \vec{l} \text{)} \\ &= \oint \vec{u} \cdot d\vec{l} + \oint (\vec{\Omega} \times \vec{r}) \cdot d\vec{l} \end{aligned}$$

scratch paper

Lets rewrite $\oint (\vec{\Omega} \times \vec{r}) \cdot d\vec{l}$ using Stokes thm.

Stokes thm: $\oint \vec{V} \cdot d\vec{l} = \iint \hat{n} \cdot (\nabla \times \vec{V}) dA$ for any vector \vec{V} .

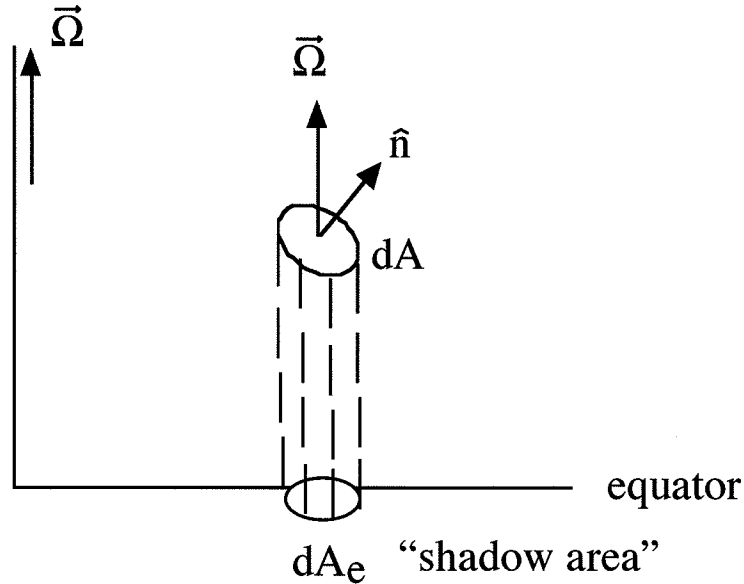
Let $\vec{V} \equiv \vec{\Omega} \times \vec{r}$. Then: $\oint (\vec{\Omega} \times \vec{r}) \cdot d\vec{l} = \iint \hat{n} \cdot \left[\nabla \times (\vec{\Omega} \times \vec{r}) \right] dA$

$$\therefore C_a = C + \iint \hat{n} \cdot \left[\nabla \times (\vec{\Omega} \times \vec{r}) \right] dA$$

\downarrow \downarrow
 rel circ $= 2\vec{\Omega}$ (done in prob set)

$$\therefore C_a = C + \iint 2\vec{\Omega} \cdot \hat{n} dA$$

$\hat{n} dA$ is tiny directed area element. Let dA_e be the projection of $\hat{n} dA$ onto the equatorial plane (plane \perp to $\vec{\Omega}$):



$$dA_e \equiv \frac{\vec{\Omega}}{\Omega} \cdot \hat{n} dA \quad \left[\frac{\vec{\Omega}}{\Omega} \text{ and } \hat{n} \text{ are unit vectors} \right]$$

mult by 2Ω

$$2\Omega dA_e = 2\vec{\Omega} \cdot \hat{n} dA$$

$$\therefore C_a = C + \iint 2\Omega dA_e \quad \text{Evaluate integral, get:}$$

$$\boxed{C_a = C + 2\Omega A_e}$$

absolute circ = relative circ + earth vort x total projected area

So Kelvin's circulation theorem says that for closed material curve moving in a frictionless, barotropic flow,

$$\text{(absolute version): } \frac{DC_a}{Dt} = 0 \quad \text{or} \quad C_a = \text{const}$$

$$\text{(relative version): } \frac{DC}{Dt} + 2\Omega \frac{DA_e}{Dt} = 0 \quad \text{or} \quad C + 2\Omega A_e = \text{const}$$

where A_e is the projection of the area enclosed by the material curve on the equatorial plane.