

LECTURE 34

The Planetary Boundary Layer (continued)

Ekman layer (continued)

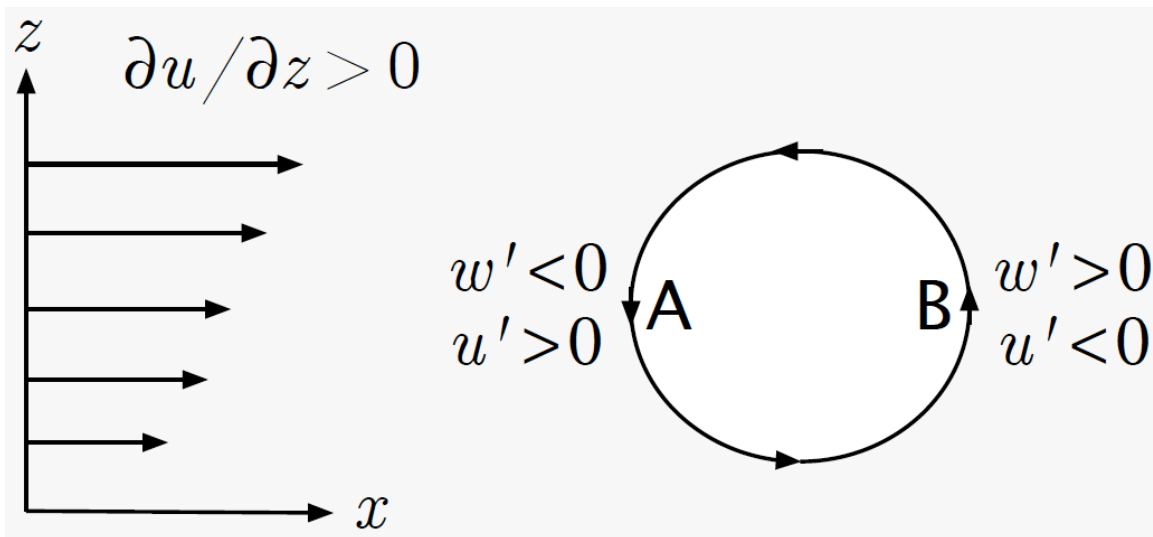
We close the system using an **eddy viscosity parameterization** (also due to Boussinesq) in which the Reynolds stresses $\overline{u'w'}$ and $\overline{v'w'}$ are set proportional to vertical gradients of the corresponding mean velocity components:

$$\overline{u'w'} = -K \frac{d\bar{u}}{dz}, \quad (33)$$

$$\overline{v'w'} = -K \frac{d\bar{v}}{dz}. \quad (34)$$

Here K is the eddy viscosity coefficient (or just eddy viscosity). **Relating Reynolds stresses to velocity gradients through an eddy viscosity coefficient** is analogous to **relating viscous shear stresses to velocity gradients through a kinematic viscosity coefficient** (covered in Dynamics I).

Does this parameterization make sense? Consider an eddy in a shear flow:



In rising branch (point B, where $w' > 0$) statistically slower air is transported upward

(since $d\bar{u}/dz > 0$, air beneath B has a smaller value of u than air at B). So u value transported past B is less than mean u at B , so $u' < 0$. **The stronger the shear, the larger this deficit is, and the larger the magnitude of u' is.** So $u'w' < 0$, with a magnitude that increases with increasing $d\bar{u}/dz$. This suggests $u'w'$ is proportional to $-d\bar{u}/dz$ (minus sign since $d\bar{u}/dz$ is positive while $u'w'$ is negative).

Similar reasoning in descending branch (point A, $w' < 0$), where faster air is transported downward ($u' > 0$) still yields $u'w' < 0$, with a magnitude that increases with increasing $d\bar{u}/dz$. Again, this suggests $u'w'$ is proportional to $-d\bar{u}/dz$.

Get same result in clockwise-spinning eddies (it's counter-clockwise in diagram).

So, for an ensemble average, we expect $\overline{u'w'} = -K \frac{d\bar{u}}{dz}$, where K is a proportionality factor that we call the eddy viscosity.

Eddy viscosity parameterization (closure) is commonly used in mesoscale and climate models – with K specified in different ways, e.g., related to wind shear and static stability, or to a predicted turbulent kinetic energy and a length scale. Here, we will simply take K to be constant (as did Ekman).

Applying (33) and (34) in (31) and (32) yields

$$0 = f(\bar{v} - v_g) + (K + \nu) \frac{d^2 \bar{u}}{dz^2},$$

$$0 = -f(\bar{u} - u_g) + (K + \nu) \frac{d^2 \bar{v}}{dz^2},$$

Daytime K ranges from 10 to 200 $\text{m}^2 \text{s}^{-1}$, while ν is $\sim 1.5 \times 10^{-5} \text{m}^2 \text{s}^{-1}$ (\sim million

to ~ 10 million times smaller than K). So we can safely neglect ν and just work with

$$0 = f(\bar{v} - v_g) + K \frac{d^2 \bar{u}}{dz^2}, \quad (35)$$

$$0 = -f(\bar{u} - u_g) + K \frac{d^2 \bar{v}}{dz^2}. \quad (36)$$

Decompose \bar{u} into a geostrophic component u_g and a part that's not geostrophic (ageostrophic wind component u_a): $\bar{u} = u_g + \bar{u}_a$. Same for \bar{v} : $\bar{v} = v_g + \bar{v}_a$. In other words, we define ageostrophic wind components by:

$$\bar{u}_a \equiv \bar{u} - u_g, \quad (37)$$

$$\bar{v}_a \equiv \bar{v} - v_g. \quad (38)$$

Since the geostrophic wind in this problem is independent of z (we showed the horizontal perturbation pgf is independent of z), we can rewrite (35) and (36) completely in terms of ageostrophic wind components:

$$0 = f\bar{v}_a + K \frac{d^2 \bar{u}_a}{dz^2}, \quad (39)$$

$$0 = -f\bar{u}_a + K \frac{d^2 \bar{v}_a}{dz^2}. \quad (40)$$

There are (at least) two different ways to solve the coupled ODEs (39) and (40):

(i) **Standard way.** "Uncouple" the equations by eliminating one variable in favor of another. For example, write \bar{v}_a in terms of \bar{u}_a . From (39): $\bar{v}_a = -(K/f) d^2 \bar{u}_a / dz^2$. Plugging this into (40) yields a 4th order ODE for just one variable:

$$\frac{d^4 \bar{u}_a}{dz^4} + \frac{f^2}{K^2} \bar{u}_a = 0.$$

Eliminating \bar{u}_a in favor of \bar{v}_a would lead to an analogous 4th order ODE for \bar{v}_a .

(ii) **Linear combination "trick"**. Combine the 2 ODEs into 1 ODE in a single **new** dependent variable, a linear combination of the original variables. If this trick works (it often doesn't), it really simplifies things. **We'll solve (39) and (40) this trick way.**

Multiply (40) by i and add the resulting equation to (39):

$$0 = f(\bar{v}_a - i\bar{u}_a) + K \frac{d^2}{dz^2}(\bar{u}_a + i\bar{v}_a), \quad (41)$$

Define a new dependent variable " M ",

$$M \equiv \bar{u}_a + i\bar{v}_a. \quad (42)$$

This simplifies last term in (41), but what about the first term? Write \bar{u}_a or \bar{v}_a in terms of M (doesn't matter which one; get same result in the end). Okay, I'll use \bar{u}_a :

$\bar{u}_a = M - i\bar{v}_a$. Plug that into first term:

$$\begin{aligned} f(\bar{v}_a - i\bar{u}_a) &= f[\bar{v}_a - i(M - i\bar{v}_a)] = f[\bar{v}_a - iM + i^2\bar{v}_a] && \text{use } i^2 = -1 \\ &= f[\bar{v}_a - iM - \bar{v}_a] = -ifM \end{aligned}$$

So first term also simplifies! So (41) reduces to:

$$0 = -ifM + K \frac{d^2M}{dz^2}. \quad (43)$$

It's a 2nd order linear constant coefficient homogeneous ODE. Seek solutions in the form of exponentials. Plug the trial solution $M \sim e^{qz}$ into (43), get:

$$\begin{aligned} 0 &= -if e^{qz} + K \frac{d^2 e^{qz}}{dz^2} \\ 0 &= -if e^{qz} + Kq^2 e^{qz} \quad \div \text{ by } e^{qz} \end{aligned}$$

$$0 = -if + Kq^2$$

$$q^2 = i \frac{f}{K} \quad \text{Take square root}$$

$$q = \pm \sqrt{i} \sqrt{\frac{f}{K}} \quad \text{We really get two possible roots (plus and minus)}$$

Use fact that $\sqrt{i} = \frac{1}{\sqrt{2}} + i \frac{1}{\sqrt{2}}$ (you'll prove it in the problem set).

$$q = \pm \left(\frac{1}{\sqrt{2}} + i \frac{1}{\sqrt{2}} \right) \sqrt{\frac{f}{K}}$$

Simplifies a bit:

$$q = \pm (1 + i) \sqrt{\frac{f}{2K}}$$

So we get two q as:

$$q_1 = (1 + i) \sqrt{\frac{f}{2K}}, \quad q_2 = -(1 + i) \sqrt{\frac{f}{2K}}. \quad (44)$$

Note: We'll restrict attention to the **Northern hemisphere**. So $f > 0$. And K is some positive constant. So $\sqrt{\frac{f}{2K}}$ is real.