

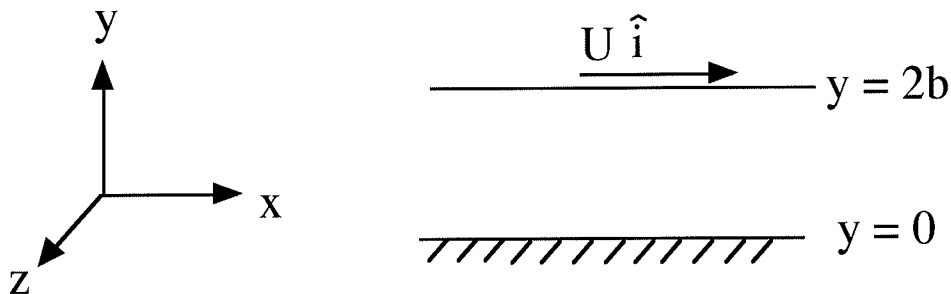
METR 5113, Advanced Atmospheric Dynamics I
 Alan Shapiro, Instructor
 Monday, 1 Rocktober 2018 (lecture 18)

Exact solutions of incompressible Navier-Stokes eq^{ns} (cont^d)

Planar Couette Flow

[Ask students to go through this Couette analysis themselves]

Again consider steady flow btw 2 infinite parallel plates. This time suppose there is no pgf but the top plate is moving with velocity $U \hat{i}$. As before, assume 2-D flow $u = u(y)$, $v = 0$, $w = 0$.



Impermeability condⁿ: $v(0) = 0$, $v(2b) = 0$. Automatically satisfied since $v = 0$ everywhere.

No-slip condⁿ on w : $w(0) = 0$, $w(2b) = 0$. Automatically satisfied since $w = 0$ everywhere.

No slip condⁿ on u : $u(0) = 0$ (fluid sticks to stationary plate)
 $u(2b) = U$ (fluid sticks to moving plate)
 We'll enforce these conditions later.

Can show that incomp condⁿ is satisfied everywhere (get $\theta = 0$). Write down N.S. eq^{ns} and slaughter terms like before but now all pgf terms are 0 (flow driven by moving plate, not pgf). Get:

$$\text{x-comp NS eq}^n: \quad \nu \frac{d^2 u}{dy^2} = 0$$

$$\text{y-comp NS eq}^n: \quad 0 = 0$$

$$\text{z-comp NS eq}^n: \quad 0 = 0$$

int. x-comp eqⁿ w.r.t. y, get

$$\frac{du}{dy} = C, \quad \text{int again w.r.t. y, get}$$

$$u = Cy + D$$

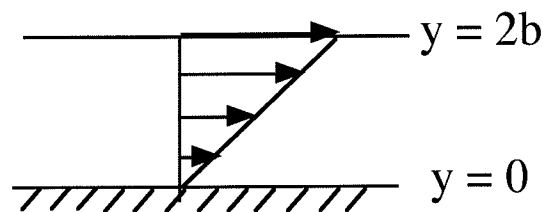
Apply no-slip condition on u on lower plate:

$$u(0) = 0 \rightarrow 0 = 0 + D \quad \therefore \boxed{D = 0}$$

Apply no-slip condition on u on upper plate:

$$u(2b) = U \rightarrow U = C \cdot 2b + D \quad \therefore \boxed{C = \frac{U}{2b}}$$

$$\therefore \boxed{u = \frac{U}{2b} y} \quad \text{linear profile}$$



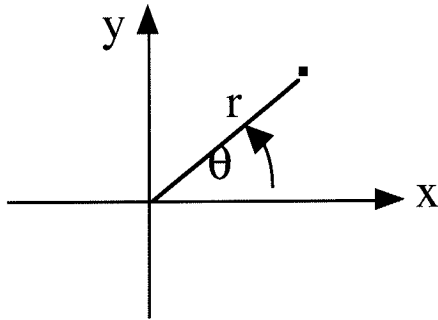
Combination Planar Poiseuille/Couette flow

Get a solⁿ for flow due to boundary translation and imposed pgf
 [You're invited to ~~a party~~ fill in the details.]

$$u = \frac{U}{2b} y + \frac{K}{\rho v} \left(\frac{y^2}{2} - by \right), \quad v = 0, \quad w = 0$$

[for picture, see Kundu, Fig. 9.4 (eds. 1-4), or Fig. 8.4 (5th ed.)]

N.S. eq^{ns} in cylindrical coords



$$x = r \cos\theta$$

$$y = r \sin\theta$$

$z \perp$ to xy plane

Cartesian

x, y, z

u, v, w

Cylindrical

r, θ, z (r : radial, θ : azimuthal)

u_r, u_θ, u_z or call them u, v, w (not Cartesian!)

r comp NS eqⁿ:

$$\frac{\partial u}{\partial t} + u \frac{\partial u}{\partial r} + \frac{v}{r} \frac{\partial u}{\partial \theta} + w \frac{\partial u}{\partial z} - \frac{v^2}{r} = -\frac{1}{\rho} \frac{\partial p'}{\partial r} + \nu \left(\nabla^2 u - \frac{2}{r^2} \frac{\partial v}{\partial \theta} - \frac{u}{r^2} \right)$$

θ -comp NS eqⁿ:

$$\frac{\partial v}{\partial t} + u \frac{\partial v}{\partial r} + \frac{v}{r} \frac{\partial v}{\partial \theta} + w \frac{\partial v}{\partial z} + \frac{uv}{r} = -\frac{1}{\rho r} \frac{\partial p'}{\partial \theta} + \nu \left(\nabla^2 v + \frac{2}{r^2} \frac{\partial u}{\partial \theta} - \frac{v}{r^2} \right)$$

z-comp NS eqⁿ:

$$\frac{\partial w}{\partial t} + u \frac{\partial w}{\partial r} + \frac{v}{r} \frac{\partial w}{\partial \theta} + w \frac{\partial w}{\partial z} = -\frac{1}{\rho} \frac{\partial p'}{\partial z} + \nu \nabla^2 w$$

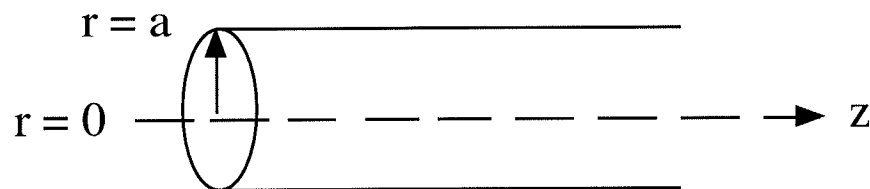
$$\text{where } \nabla^2 = \frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial}{\partial r} \right) + \frac{1}{r^2} \frac{\partial^2}{\partial \theta^2} + \frac{\partial^2}{\partial z^2}$$

$$\text{Incomp condⁿ: } \frac{1}{r} \frac{\partial}{\partial r} (r u) + \frac{1}{r} \frac{\partial v}{\partial \theta} + \frac{\partial w}{\partial z} = 0$$

Poiseuille flow

Consider steady unidirectional pressure-driven flow in a pipe of circular cross-section.

Use cylindrical coords. Put z-axis down center of pipe. Let pipe radius be a.



Assume unidirectional flow such that:

$$\vec{u} = w \hat{k}, \quad \begin{array}{l} \mathbf{u} = 0, \\ \text{(no radial flow)} \end{array}, \quad \begin{array}{l} \mathbf{v} = 0 \\ \text{(no azimuthal flow)} \end{array}$$

Also assume flow is symmetric about pipe axis and indep of downstream direction z. $\therefore w = w(r)$

Impermeability condition: flow component normal to pipe should be 0 (on pipe), i.e., $u(a) = 0$. It's satisfied since $u = 0$ everywhere.

No-slip condition on pipe surface (involves v and w):

$v(a) = 0$ satisfied since $v = 0$ everywhere

$w(a) = 0$... need to return to this one later.

$$\text{Incomp cond}^n: \quad \frac{1}{r} \frac{\partial}{\partial r} (r u) + \frac{1}{r} \frac{\partial v}{\partial \theta} + \frac{\partial w}{\partial z} = 0$$

$\begin{matrix} 0 & 0 & 0 \\ \text{since } u = 0 & v = 0 & w \text{ indep of } z \end{matrix}$

get: $0 + 0 + 0 = 0$. okee

N.S. eq^{ns} for this case reduce to:

$$\text{r comp:} \quad 0 = -\frac{1}{\rho} \frac{\partial p'}{\partial r} \quad \rightarrow \quad p' = f(\theta, z)$$

$$\theta\text{-comp:} \quad 0 = -\frac{1}{\rho r} \frac{\partial p'}{\partial \theta} \quad \rightarrow \quad p' = g(r, z)$$

$$\text{z-comp:} \quad 0 = -\frac{1}{\rho} \frac{\partial p'}{\partial z} + \frac{v}{r} \frac{\partial}{\partial r} \left(r \frac{\partial w}{\partial r} \right)$$

Since $f(\theta, z) = g(r, z)$ must have $f(\theta, z) = f(z)$ and $g(r, z) = g(z)$
 -- only z dependence is possible. So $p' = p'(z)$.

Rewrite z-comp eqⁿ with ordinary derivatives,

$$0 = -\frac{1}{\rho} \frac{dp'}{dz} + \frac{v}{r} \frac{d}{dr} \left(r \frac{dw}{dr} \right)$$

$\begin{matrix} \text{at most a } f^n \text{ of } z & \text{at most a } f^n \text{ of } r \end{matrix}$

But a f^n of z can't equal a f^n of r unless the functions are const.

Mult by r/v :

$$\frac{d}{dr} \left(r \frac{dw}{dr} \right) = \frac{r}{\rho v} \frac{dp'}{dz} = \frac{r}{\mu} \frac{dp'}{dz} \quad \text{int w.r.t. } r,$$

$$r \frac{dw}{dr} = \frac{r^2}{2\mu} \frac{dp'}{dz} + A \quad \div \text{ by } r,$$

$$\frac{dw}{dr} = \frac{r}{2\mu} \frac{dp'}{dz} + \frac{A}{r} \quad \text{int w.r.t } r,$$

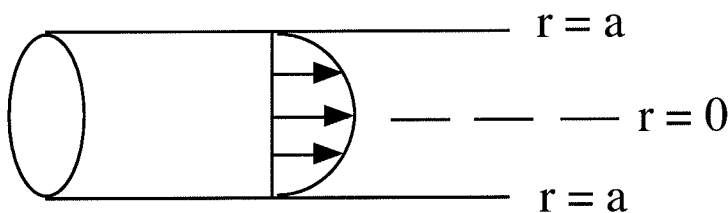
$$w(r) = \frac{r^2}{4\mu} \frac{dp'}{dz} + A \ln r + B$$

Want w to be finite along centerline $r=0$ (a finiteness "boundary condition") \therefore take $\boxed{A = 0}$ to avoid singularity.

No-slip b.c. on pipe wall: $w(a) = 0$.

$$\therefore 0 = \frac{a^2}{4\mu} \frac{dp'}{dz} + \underset{0}{\downarrow} A \ln a + B, \quad \therefore \boxed{B = -\frac{a^2}{4\mu} \frac{dp'}{dz}}$$

$$\therefore \boxed{w(r) = -\frac{1}{4\mu} \frac{dp'}{dz} (a^2 - r^2)} \quad \text{a parabolic profile}$$



Volume flux through pipe:

$$Q \equiv \int \vec{u} \cdot \hat{n} dA = \int_0^{2\pi} \int_0^a w r dr d\theta = 2\pi \int_0^a w r dr$$

$$= -\frac{2\pi}{4\mu} \frac{dp'}{dz} \left[\int_0^a (a^2 - r^2) r dr \right] \rightarrow a^4/4$$

$$\therefore \boxed{Q = -\frac{\pi}{8\mu} \frac{dp'}{dz} a^4} \quad \text{Hagen-Poiseuille law}$$

- obtained theoretically by Stokes but he didn't publish it because it didn't agree w/ his experiments. His experiments were turbulent but the theory is for laminar flow. [see pg 92 of Truesdell's "Six lectures on modern natural philosophy"]

- HP law discovered experimentally by Hagen and Poiseuille. [1993 Ann. Rev. Fluid Mech. article on Poiseuille's experiments]

- Experimental confirmation of HP law confirms appropriateness of NS eq^{ns} as governing eq^{ns} of motion (at least for liquid). Confirms $F = ma$, Newtonian hypothesis and no slip condition.

- volume flux is tremendously sensitive to pipe radius ($Q \propto a^4$)

- $\frac{dp'}{dz} \propto \frac{Q}{a^4}$. In case of blood flow, body tries to maintain a fixed

Q . If $a \downarrow$ (e.g. due to cholesterol deposits) then $\frac{dp'}{dz}$ goes way up to maintain Q . This is why cholesterol deposits are often associated w/ high blood pressure.

HP law breaks down when flow becomes turbulent (as in Stokes case). Then N.S. eqⁿ are still valid but our starting assumptions are violated (flow is unsteady, not unidirectional, no symmetry).