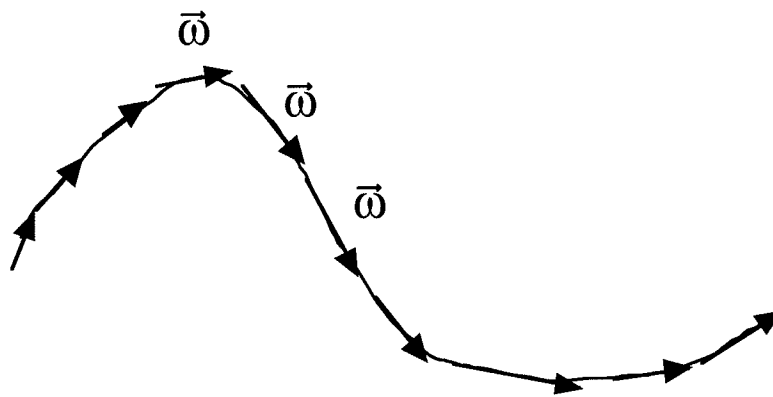


METR 5113, Advanced Atmospheric Dynamics I
 Alan Shapiro, Instructor
 Wednesday, 24 October 2018 (lecture 27)

Kinematics of Vorticity

$$\text{vorticity } \vec{\omega} \equiv \nabla \times \vec{u}$$

A line that is everywhere tangential to the local vorticity vector is a vortex line (or vortex filament).



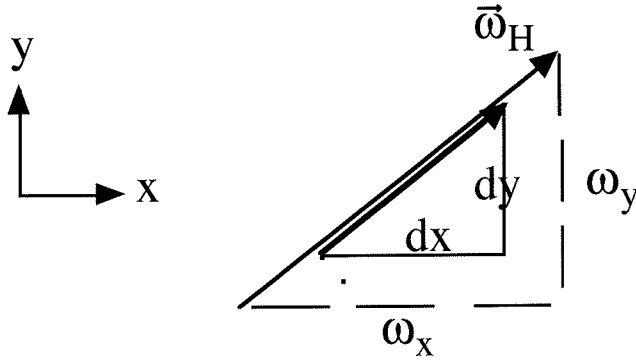
Note: A vortex line is not the same thing as a line vortex ["line vortex" is a vr-vortex or name given to a concentrated vortex -- vorticity concentrated in a small tube-like volume]

ODEs for vortex lines are analogous to ODEs for streamlines.
 Derive them analytically by expanding out

$$\vec{dx} \times \vec{\omega} = 0, \quad [\text{for streamlines we expanded out } \vec{dx} \times \vec{u} = 0]$$

where $\vec{dx} = dx \hat{i} + dy \hat{j} + dz \hat{k}$ is a chunk of the vortex line.

Or can derive them geometrically by considering the diagram:



where $\vec{\omega}_H \equiv \omega_x \hat{i} + \omega_y \hat{j}$

so $\frac{dy}{dx} = \frac{\omega_y}{\omega_x}$, similarly: $\frac{dz}{dx} = \frac{\omega_z}{\omega_x}$. Can put them in the form:

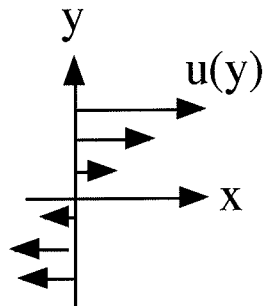
$$\boxed{\frac{dy}{\omega_y} = \frac{dx}{\omega_x} = \frac{dz}{\omega_z}}$$

or can introduce a parameter "s" such that $\frac{dy}{\omega_y} = \frac{dx}{\omega_x} = \frac{dz}{\omega_z} = ds$,
from which follows parametric form of odes for the vortex line:

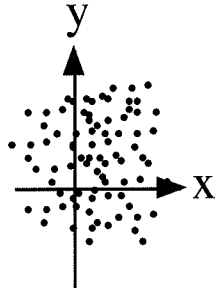
$$\boxed{\frac{dx}{ds} = \omega_x, \quad \frac{dy}{ds} = \omega_y, \quad \frac{dz}{ds} = \omega_z}$$

Vortex lines are present whenever there is vorticity in flow
(don't need to have a vortex).

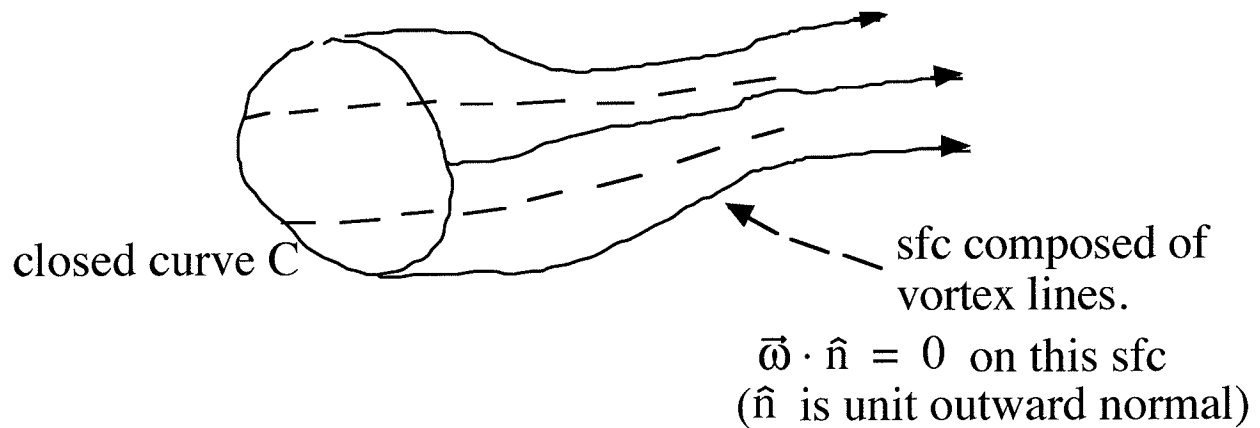
e.g. shear flow $u = u(y)$, $v = 0$, $w = 0$



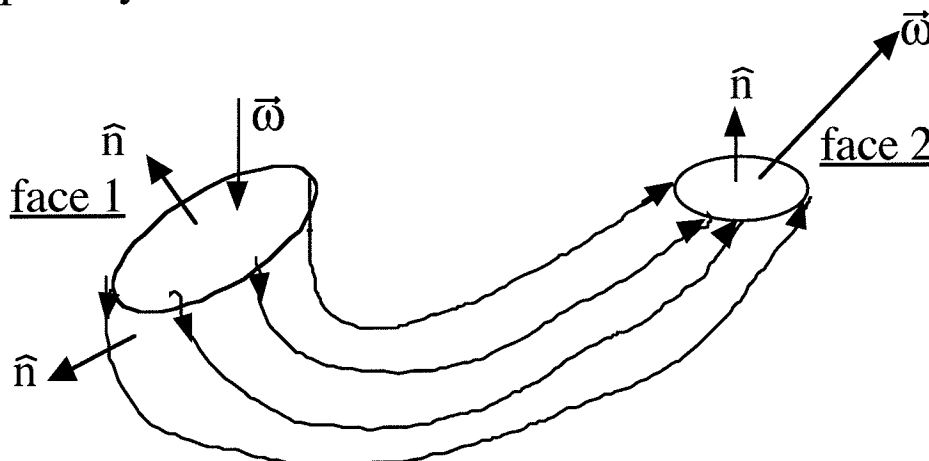
In this case vorticity is all in vertical dirⁿ, $\vec{\omega} = -\frac{\partial u}{\partial y} \hat{k}$ (in $-\hat{k}$ dirⁿ or $+\hat{k}$ dirⁿ) so vortex lines are all in vertical dirⁿ.



Vortex lines passing through any closed curve form a tubular sfc known as a vortex tube [analogous to construction of streamtube from streamlines passing through a closed curve]



Recall $\nabla \cdot \vec{\omega} = 0$ for all flows (done in prob set) $\therefore \int \nabla \cdot \vec{\omega} dV = 0$ for any fluid volume. In particular, consider the volume occupied by a chunk of a vortex tube.



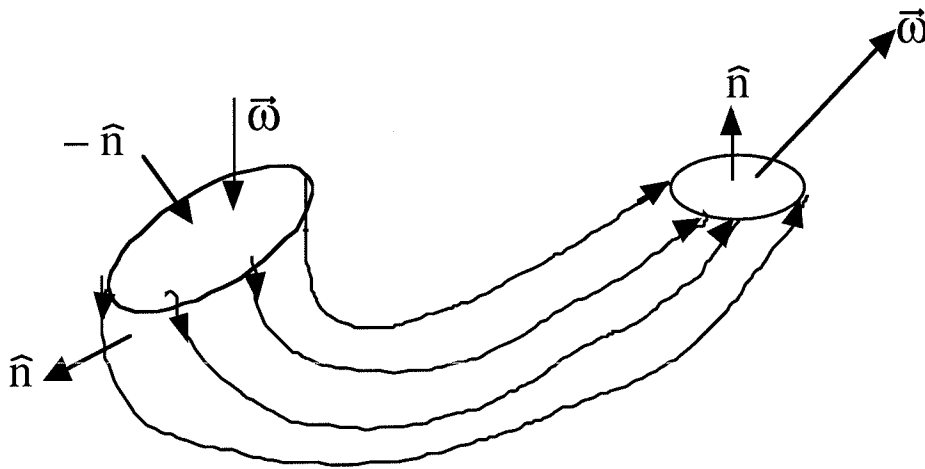
But div thm says $\int \nabla \cdot \vec{\omega} dV = \int \vec{\omega} \cdot \hat{n} dA$. Since l.h.s. is 0, the r.h.s must be 0. So $\int \vec{\omega} \cdot \hat{n} dA = 0$. This area integral is over closed surface bounding chunk of tube (sides + two end faces).

$$\therefore \int_{\text{face 1}} \vec{\omega} \cdot \hat{n} dA + \int_{\text{face 2}} \vec{\omega} \cdot \hat{n} dA + \int_{\text{sides}} \vec{\omega} \cdot \hat{n} dA = 0$$

0 on sides of tube
↑

$$\therefore - \int_{\text{face 1}} \vec{\omega} \cdot \hat{n} dA = \int_{\text{face 2}} \vec{\omega} \cdot \hat{n} dA$$

$$\therefore \int_{\text{face 1}} \vec{\omega} \cdot (-\hat{n}) dA = \int_{\text{face 2}} \vec{\omega} \cdot \hat{n} dA$$



[now use fact that "average = integral divided by interval"]

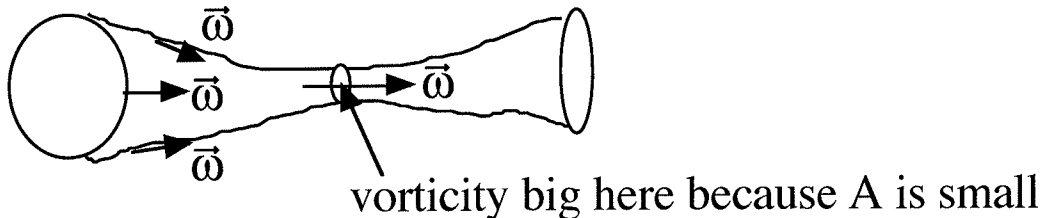
$$\therefore A_1 \left[\frac{1}{A_1} \int \vec{\omega} \cdot (-\hat{n}) dA \right] = A_2 \left[\frac{1}{A_2} \int \vec{\omega} \cdot \hat{n} dA \right]$$

average inward comp
of vorticity on face 1

average outward comp
of vorticity on face 2

More generally, $A\bar{\omega}$ has same value on any x-section through a given vortex tube. So $A\bar{\omega} = \text{const}$ for a vortex tube, where A

is cross-section area through tube and $\bar{\omega}$ is ave vorticity comp \perp to cross-section area. $A\bar{\omega}$ is "strength" of vortex tube. So vortex tube strength is constant -- indep of where cross-section is taken.



Rewrite $A\bar{\omega} = \text{const}$ using Stokes Th^m, get: $\oint \vec{u} \cdot d\vec{l} = \text{const}$. Here the curve is the intersection of the tube and cross-section area. So circulation is the same for any cross-section along vortex tube.

These results are kinematic relations valid at a fixed time. How does vortex tube strength (or circulation) change with time? Need to consider dynamics.

Vorticity and Circulation Dynamics (Ch5 Kundu 1st-6th ed)

Kelvin's Circulation Th^m

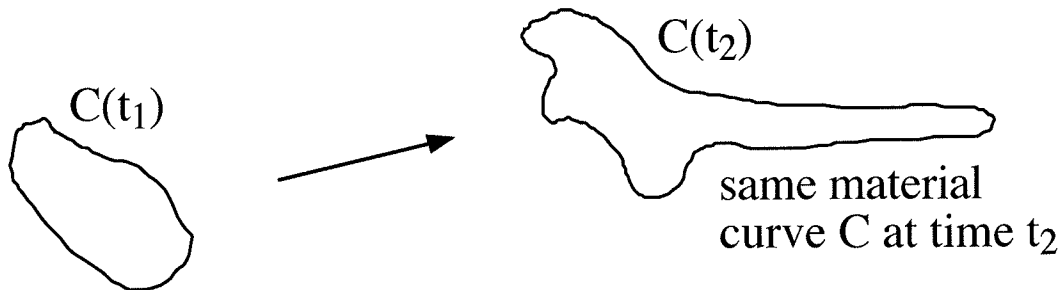
Assume flow is:

- (1) inviscid
- (2) subject to conservative body forces (force can be expressed as gradient of something -- as in gravity force)
- (3) barotropic, $\rho = \rho(p)$
- (4) described in an inertial (non-accelerating) ref frame

Appropriate eq^{ns} of motion are Euler eq^{ns}:

$$\frac{D\vec{u}}{Dt} = -\frac{1}{\rho} \nabla p + \vec{g}, \quad \text{where } \vec{g} = -\nabla gz$$

Consider an arbitrary closed curve C (arbitrary at a particular time, but once you've defined it, you're stuck with it). Curve is composed of air parcels. Follow curve as it moves around. C is always composed of same parcels -- same material -- it's a material curve.



Let $\Gamma(t) \equiv \oint \vec{u} \cdot d\vec{l}$ be circulation around C .

To see how Γ changes with time, derive a formula for $\frac{D\Gamma}{Dt}$, rate of change of circulation around closed material curve.