

METR 5113, Advanced Atmospheric Dynamics I
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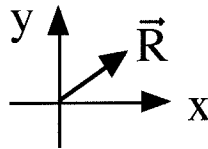
Eq^{ns} of motion (and vort eqⁿ, etc) in rotating ref frame

N-S eqn in Rot Frame is:

$$\frac{D\vec{u}}{Dt} = -\frac{1}{\rho} \nabla p - 2\vec{\Omega} \times \vec{u} + \Omega^2 \vec{R} + \vec{g} + \nu \nabla^2 \vec{u}$$

Coriolis force centrifugal force

Now lets rewrite $\Omega^2 \vec{R}$ as gradient of a scalar potential function.
 Orient Cartesian coord system s.t. xy plane contains \vec{R} :



$$\vec{R} = x \hat{i} + y \hat{j}$$

$$R \equiv |\vec{R}| = \sqrt{x^2 + y^2}$$

$$\therefore R^2 = x^2 + y^2$$

$$\therefore \nabla R^2 = \nabla x^2 + \nabla y^2 = 2x \hat{i} + 2y \hat{j} = 2(x\hat{i} + y\hat{j}) = 2\vec{R}$$

$$\therefore \vec{R} = \nabla R^2 / 2$$

$$\therefore \Omega^2 \vec{R} = \nabla \left[\Omega^2 R^2 / 2 \right] \rightarrow \text{centrifugal potential}$$

Gravity can be written as gradient of a gravitational potential:

$$\vec{g} = -\nabla\Pi$$

So sum of gravity and centrifugal force can be written as gradient of a potential:

$$\vec{g} + \Omega^2\vec{R} = -\nabla\Pi + \nabla\Omega^2R^2/2 = -\nabla(\Pi - \Omega^2R^2/2)$$

redefine \vec{g} to be "effective gravity":

$$\begin{aligned} \vec{g}_{\text{effective gravity}} &= \vec{g}_{\text{gravity}} + \Omega^2\vec{R}_{\text{centrifugal force}} \\ &= -\nabla g_Z \rightarrow \text{local height above an equipotential surface} \\ &\quad \downarrow \\ &\quad \text{accel due to effective gravity} \end{aligned}$$

Note that $\nabla \times \vec{g} = 0$ (for effective \vec{g})

How does vorticity as observed in a fixed (inertial) ref frame differ from vort obs in rotating (non-inertial) ref frame?

$$\begin{aligned} \vec{\omega}_F &\equiv \nabla \times \vec{u}_F = \nabla \times (\vec{u}_R + \vec{\Omega} \times \vec{r}) \\ \text{abs vort} & \\ &= \nabla \times \vec{u}_R + \nabla \times (\vec{\Omega} \times \vec{r}) \\ &= \vec{\omega}_R + \nabla \times (\vec{\Omega} \times \vec{r}) \\ &= \vec{\omega}_R + \underbrace{\vec{\Omega} \nabla \cdot \vec{r}}_3 + \underbrace{(\vec{r} \cdot \nabla)\vec{\Omega}}_0 - \underbrace{\vec{r} \nabla \cdot \vec{\Omega}}_0 - (\vec{\Omega} \cdot \nabla)\vec{r} \end{aligned}$$

$$\begin{aligned}
&= \vec{\omega}_R + 3\vec{\Omega} - \left(\Omega_x \left[\frac{\partial \vec{r}}{\partial x} \right] \rightarrow \hat{i} + \Omega_y \left[\frac{\partial \vec{r}}{\partial y} \right] \rightarrow \hat{j} + \Omega_z \left[\frac{\partial \vec{r}}{\partial z} \right] \rightarrow \hat{k} \right) \\
&= \vec{\omega}_R + 3\vec{\Omega} - \vec{\Omega}
\end{aligned}$$

$$\therefore \boxed{\vec{\omega}_F = \vec{\omega}_R + 2\vec{\Omega}}$$

absolute vorticity
relative vorticity
earth vorticity

Now recast other previous equations in rot ref frame:

Can show Bernoulli's eqⁿ for steady, inviscid, barotropic flow is:

$$\frac{q^2}{2} + \int \frac{dp}{\rho} + gz = C \quad \text{along a streamline}$$

Same eqⁿ as before but with redefined g, z . q is relative speed (speed obs in rotating ref frame).

Bernoulli's eqn for irrotational, inviscid barotropic flow (possibly unsteady) will also be same as before provided "irrotational" is taken to mean the absolute vorticity is 0.

Circulation th^{ms}

In fixed frame Kelvin's th^m: $D\Gamma_F / Dt = 0$ for closed material curve in inviscid, barotropic flow.

$$\therefore \Gamma_F = C, \text{ or: } \oint \vec{u}_F \cdot d\vec{l} = C$$

sub in $\vec{u}_F = \vec{u}_R + \vec{\Omega} \times \vec{r}$,

$$\oint \vec{u}_R \cdot d\vec{l} + \oint (\vec{\Omega} \times \vec{r}) \cdot d\vec{l} = C$$

$$\Gamma_R, \text{ relative} + \text{circulation associated} = C$$

circulation w/ solid body rot.

Apply Stokes thm to 2nd term.

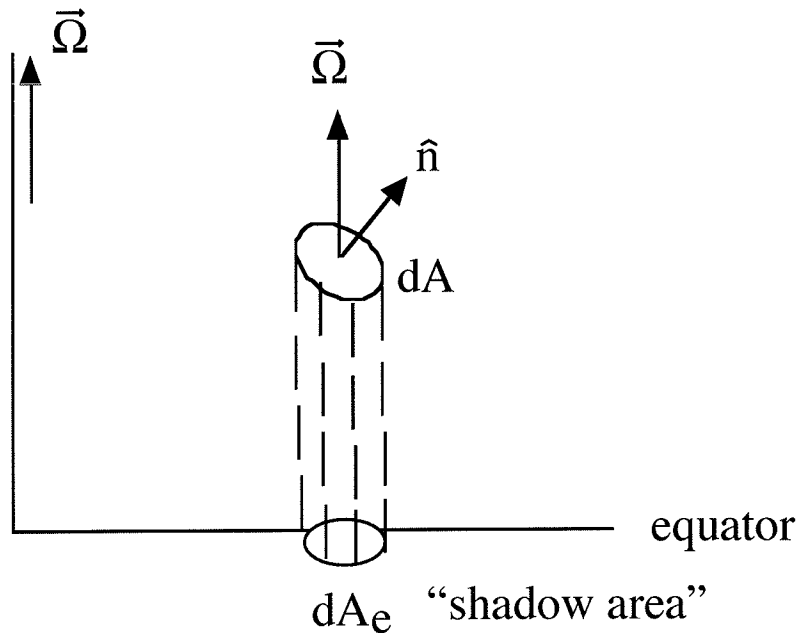
$$\Gamma_R + \int [\nabla \times (\vec{\Omega} \times \vec{r})] \cdot \hat{n} dA = C$$

↓

$2\vec{\Omega}$ (already showed it)

$$\Gamma_R + \int 2\vec{\Omega} \cdot \hat{n} dA = C$$

Rewrite integral in terms of "projected area" or "shadow area."
Consider tiny directed area element $\hat{n} dA$. Let dA_e be the projection of $\hat{n} dA$ onto the equatorial plane (plane \perp to $\vec{\Omega}$).



$$dA_e \equiv \left(\frac{\vec{\Omega}}{\Omega} \right) \cdot \hat{n} dA$$

unit vector

mult by Ω

$$\Omega dA_e = \vec{\Omega} \cdot \hat{n} dA \quad [\text{rhs is in Kelvin's thm}]$$

So Kelvin's thm in rot frame is: $\Gamma_R + \int 2\Omega dA_e = C$, or

$$\boxed{\Gamma_R + 2\Omega A_e = C} \quad \text{or} \quad \boxed{\frac{D\Gamma_R}{Dt} + 2\Omega \frac{DA_e}{Dt} = 0}$$

relative circ + earth vort x total projected area is conserved following motion of a material curve.

If flow is baroclinic then circ thm in inertial frame becomes,

$$\frac{D\Gamma_F}{Dt} = - \oint \frac{dp}{\rho}$$

and in rot frame is:

$$\boxed{\frac{D\Gamma_R}{Dt} + 2\Omega \frac{DA_e}{Dt} = - \oint \frac{dp}{\rho}} \quad \text{Bjerknes Circulation Thm}$$

Helmholtz Thm in rotating ref frame:

Absolute vortex lines (lines that are everywhere tangent to absolute vort vectors) move w/ the flow.

Vorticity eqn in rotating ref frame:

$$\frac{\partial \vec{\omega}}{\partial t} + (\vec{u} \cdot \nabla) \vec{\omega} = \left[(\vec{\omega} + 2\vec{\Omega}) \cdot \nabla \right] \vec{u} + \frac{1}{\rho^2} \nabla \rho \times \nabla p + \nu \nabla^2 \vec{\omega}$$

Ertel's Pot Vort Thm in rot ref frame:

$$\frac{D}{Dt} \left[\frac{(\vec{\omega} + 2\vec{\Omega}) \cdot \nabla \lambda}{\rho} \right] = 0$$