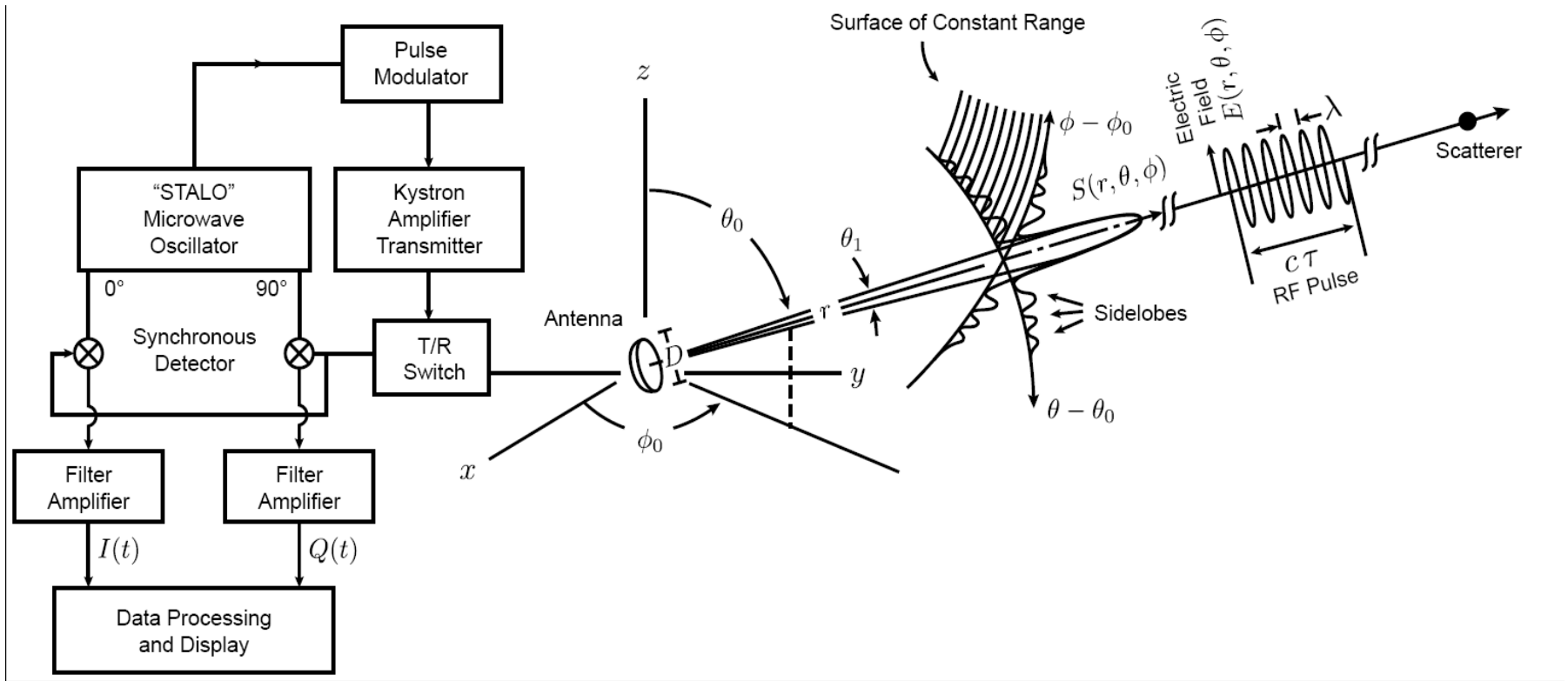


Review

Doppler Radar (Fig. 3.1) A simplified block diagram



$$E_i = \frac{A_i(\theta, \varphi)}{r} \exp \left[j2\pi f \left(t - \frac{r}{c} \right) + j\psi_t \right]$$

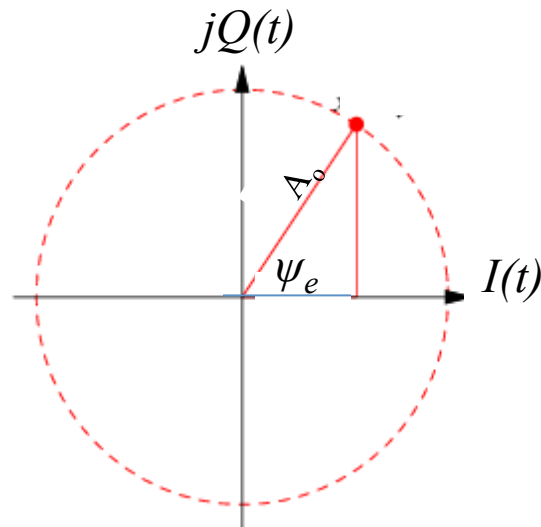
Electric field incident on scatterer

$$E_r = \frac{A_r(\theta, \varphi)}{r^2} \exp \left[j2\pi f \left(t - \frac{2r}{c} \right) + j\psi_t \right]$$

Reflected electric field incident on antenna

$$V_i = A_i \exp \left[j2\pi f t - j \frac{4\pi r}{\lambda} + j\psi_t \right]$$

Voltage input to the synchronous detectors;
This pair of detectors shifts the frequency f to 0



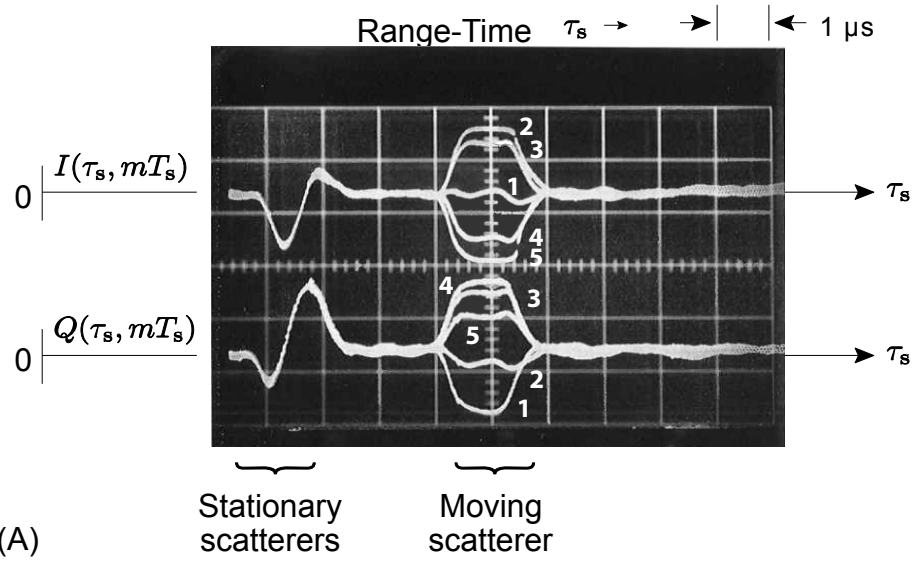
Complex plane
(Phasor diagram)

$$V_o = I + jQ \propto A_o \exp \left[-j4\pi r / \lambda + j\psi_t \right]$$

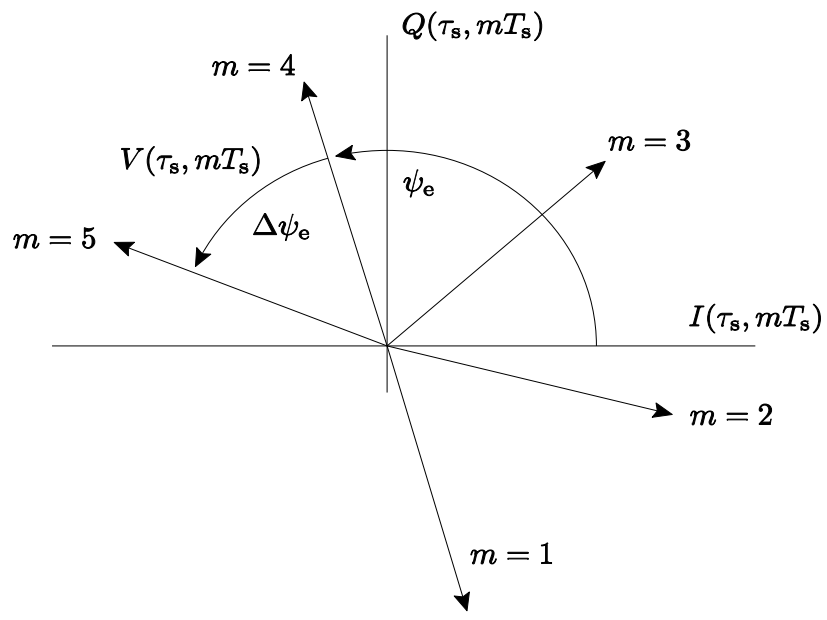
Echo voltage V_o at the output of the detectors and filters .
The echo amplitude is A_o and phase is

$$\psi_e = \left(-4\pi r / \lambda \right) + \psi_t$$

If the range r of the scatterer is fixed, the phasor (A_o, ψ_e) is fixed (i.e., no change in A_o nor ψ_e . But if scatterer has a radial velocity, phasor (A_o, ψ_e) rotates about the origin at the Doppler frequency f_d .

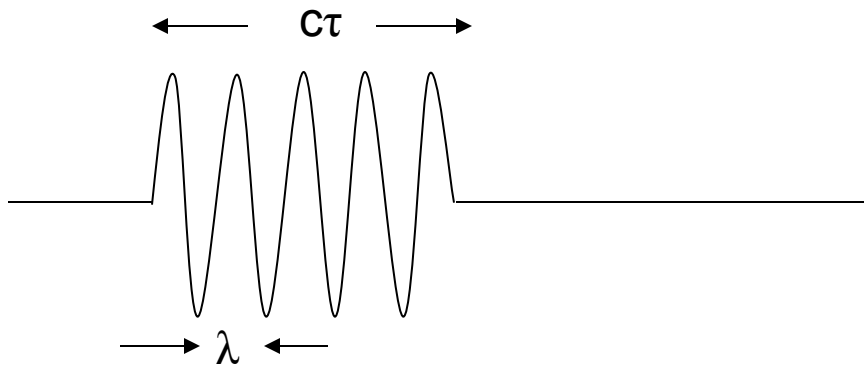
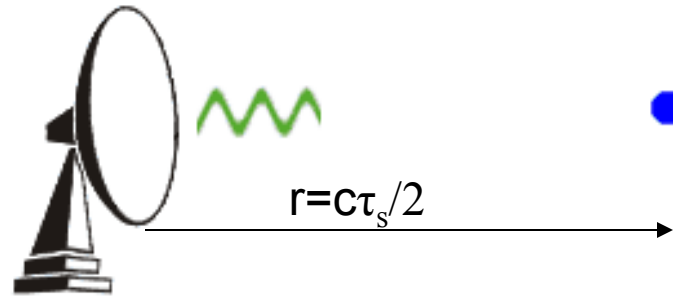


(A)



(B)

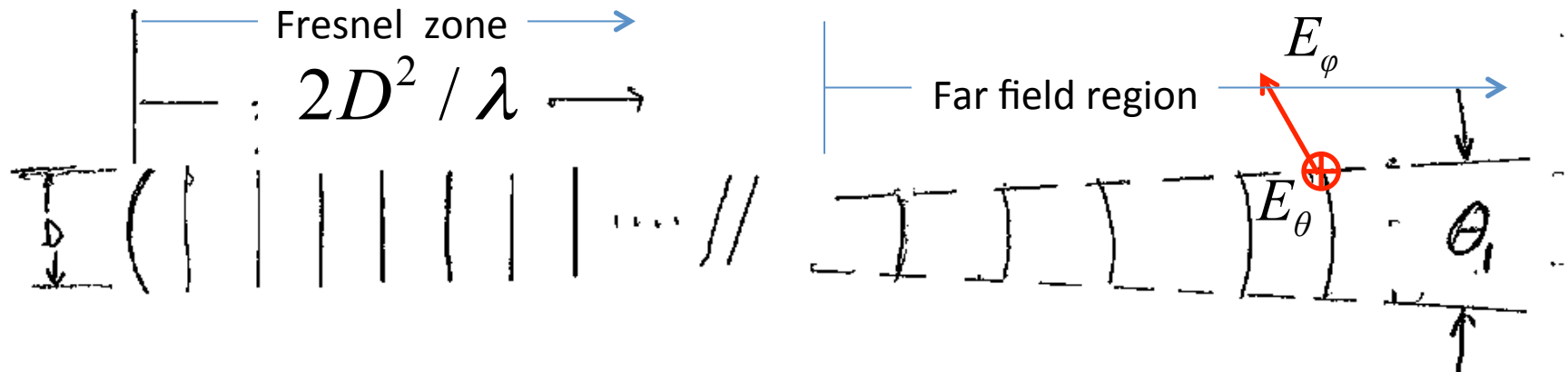
Pulsed Radar Principle



c = speed of microwaves
= c_h for H and = c_v for V waves
 τ = pulse length
 λ = wavelength
= λ_h for H and λ_v for V waves
 τ_s = time delay between
transmission of a pulse and
reception of an echo.

Angular Beam Formation

(the transition from a circular beam of constant diameter to an angular beam of constant angular width)



$$2D^2 / \lambda ; 1.5 \text{ km};$$

$$\text{WSR-88D: } D ; 8.53 \text{ m}; \lambda = 10 \text{ cm}$$

$$\theta_1 = 1.27 \lambda / D \text{ (radians)}$$

Antenna (directive) Gain g_t

The defining equation:

$$S_i = \frac{P_t}{4\pi r^2} g_t f^2(\theta, \phi) \quad \text{Eq. (3.4)}$$

S_i (W m⁻²) = Power density incident on a scatterer

r = range to measurement (m)

$f^2(\theta, \phi)$ = radiation pattern = 1 on beam axis

P_t = transmitted power (W)

Backscattering Cross Section, σ_b for a Spherical Particle

Rayleigh condition on a spherical particle of diameter D :

$$D < \lambda / 16; \quad \lambda \equiv \text{wavelength}$$

$$\sigma_b = \frac{\pi^5}{\lambda^4} |K_m|^2 D^6;$$

$$K_m \equiv \frac{m^2 - 1}{m^2 + 2}; \text{ Dielectric Factor of the medium filling the sphere; Eq.3.6}$$

$m = n - jn\kappa$ = the complex index of refraction

$$|K_m|^2 \rightarrow |K_w|^2 = 0.93 \quad \text{for water, and}$$

$$|K_m|^2 \rightarrow |K_i|^2 = 0.18 \quad \text{for ice (density = } 0.917 \text{ g m}^{-3}\text{)}$$

Backscattered Power Density Incident on Receiving Antenna

$$S_r(r, \theta, \phi) = \frac{\overbrace{P_t g_t f^2(\theta, \phi)}^{S_i}}{4\pi r^2 l} \cdot \sigma_b \cdot \frac{1}{4\pi r^2 l} \quad (3.13a)$$

where l is the loss factor (due to attenuation)

$$l = \exp \left(\int_0^r (k_g + k) dr \right) \quad (3.13b)$$

Echo Power P_r Received

$$P_r = S_r(r, \theta, \phi) A_e(\theta, \phi) \quad (3.20)$$

A_e is the effective area of the receiving antenna for radiation from the θ, ϕ direction. It is shown that:

$$A_e = g_r f_r^2(\theta, \phi) \lambda^2 / 4\pi \quad (3.21)$$

If the transmitting antenna is the same as the receiving antenna then:

$$g_r f_r^2(\theta, \phi) = g_t f_t^2(\theta, \phi) \equiv g f^2(\theta, \phi)$$

The Radar Equation

(point scatterer/discrete object)

$$P_r = \frac{P_t g f^2(\theta, \varphi)}{4\pi r^2 l} \cdot \frac{\sigma_b}{4\pi r^2 l} \cdot \frac{g \lambda^2 f^2(\theta, \varphi)}{4\pi} \quad (3.24)$$

Example:

$$\lambda = 0.1 \text{ m}; \quad r = 20 \text{ km} (2 \times 10^4 \text{ m}); \quad P_r(\text{min}) = 10^{-14} \text{ (W)};$$

$$P_t = 10^6 \text{ (W; peak)}; \quad g = 3 \times 10^4; \quad l = 1 \text{ (no path loss)}$$

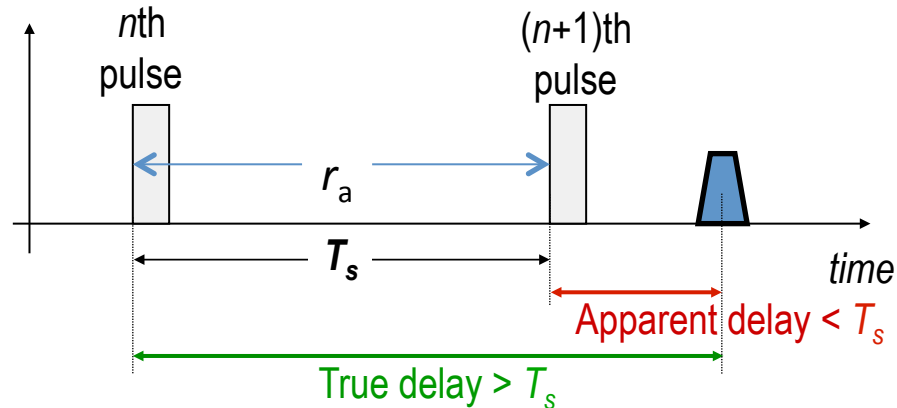
Calculating the minimum detectable backscattering σ_b :

$$\sigma_b(\text{min}) = 2 \times 10^{-7} \text{ m}^2 = \sigma_b \text{ for a 6.3 mm drop!}$$

Unambiguous Range r_a

- If targets are located beyond $r_a = cT_s/2$, their echoes from the n^{th} transmitted pulse are received after the $(n+1)^{\text{th}}$ pulse is transmitted. Thus, they appear to be closer to the radar than they really are!
 - This is known as **range folding**

- $T_s = \text{PRT}$



- **Unambiguous range:** $r_a = cT_s/2$
 - Echoes from scatterers between 0 and r_a are called **1st trip** echoes,
 - Echoes from scatterers between r_a and $2r_a$ are called **2nd trip** echoes,
 - Echoes from scatterers between $2r_a$ and $3r_a$ are called **3rd trip** echoes, etc

Unambiguous Velocity



- A pulsed Doppler radar measures radial Doppler velocity by keeping track of phase changes between samples that are T_s (pulse repetition time) apart
- Recall that echo phase shift is $\psi_e = -4\pi r/\lambda$. Then, the phase change from pulse to pulse is $\Delta\psi_e = -4\pi\Delta r/\lambda = -4\pi v_r T_s/\lambda$
 - Note that only phase changes between $-\pi$ and π can be unambiguously resolved
- Therefore, the unambiguous velocity is:
 - $4\pi v_a T_s/\lambda = \pi \Rightarrow v_a = \lambda/4T_s$
 - This is related to the **Nyquist** sampling theorem:
Doppler velocities outside the $\pm v_a$ interval will be aliased!

$\Delta r = v_r T_s$ is the change in range of the scatterer between successive transmitted pulses

Another PRT Trade-Off

- Correlation of pairs: $\rho(T_s) = \exp \left[-8 \left(\pi \sigma_v T_s / \lambda \right)^2 \right]$
 - This is a measure of signal coherency
- Accurate measurement of power requires long PRTs
 - $\lim_{T_s \rightarrow \infty} \rho(T_s) = 0$
 - More **independent samples** (low coherency)
- But accurate measurement of velocity requires short PRTs
 - $\lim_{T_s \rightarrow 0} \rho(T_s) = 1$
 - High correlation between sample pairs (high coherency)
 - Yet a large number of **independent sample pairs** are required

Signal Coherency

- How large a T_s can we pick?

- Correlation between $m = 1$ pairs of echo samples is:

$$\rho(T_s) = \exp\left[-8(\pi \sigma_v T_s / \lambda)^2\right]$$

- Correlated pairs: $\rho(T_s) \approx 1 \Rightarrow \frac{\pi \sigma_v T_s}{\lambda} \ll 1 \Rightarrow \frac{\lambda}{\pi T_s} \gg \sigma_v$

(i.e., Spectrum width σ_v must be much smaller than unambiguous velocity $v_a = \lambda/4T_s$)

- Increasing T_s decreases correlation exponentially

- $\text{Var}[\hat{v}]$ and $\text{Var}[\hat{\sigma}_v]$ also increases exponentially!

- Pick a threshold:

- $\rho(T_s) \geq e^{-0.5} \Rightarrow -8(\pi \sigma_v T_s / \lambda)^2 = 0.5 \Rightarrow \sigma_v \leq v_a / \pi$

- Violation of this condition results in very large errors of estimates!

Signal Coherency and Ambiguities

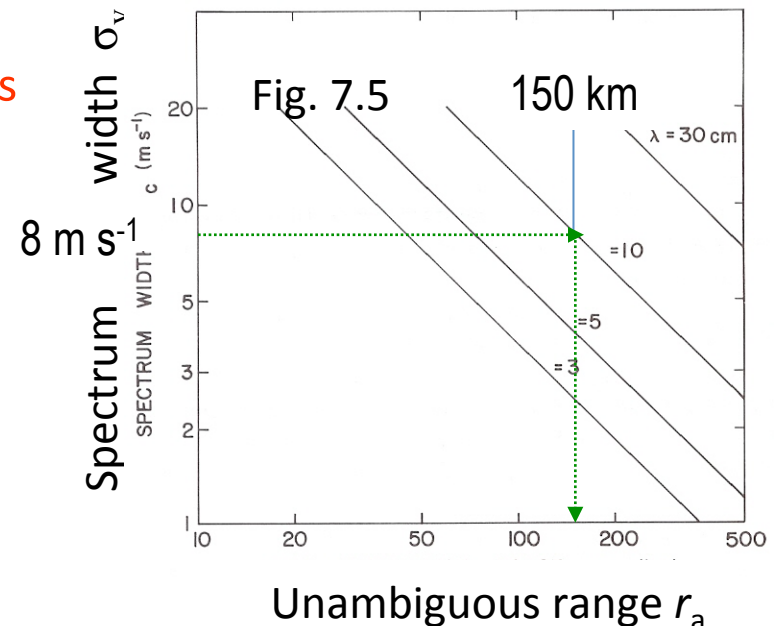
- Range and velocity dilemma: $r_a v_a = c\lambda/8$
- Signal coherency: $\sigma_v \leq v_a/\pi$

- r_a constraint: $r_a \leq \frac{c\lambda}{8\pi\sigma_v}$ Eq. (7.2c)

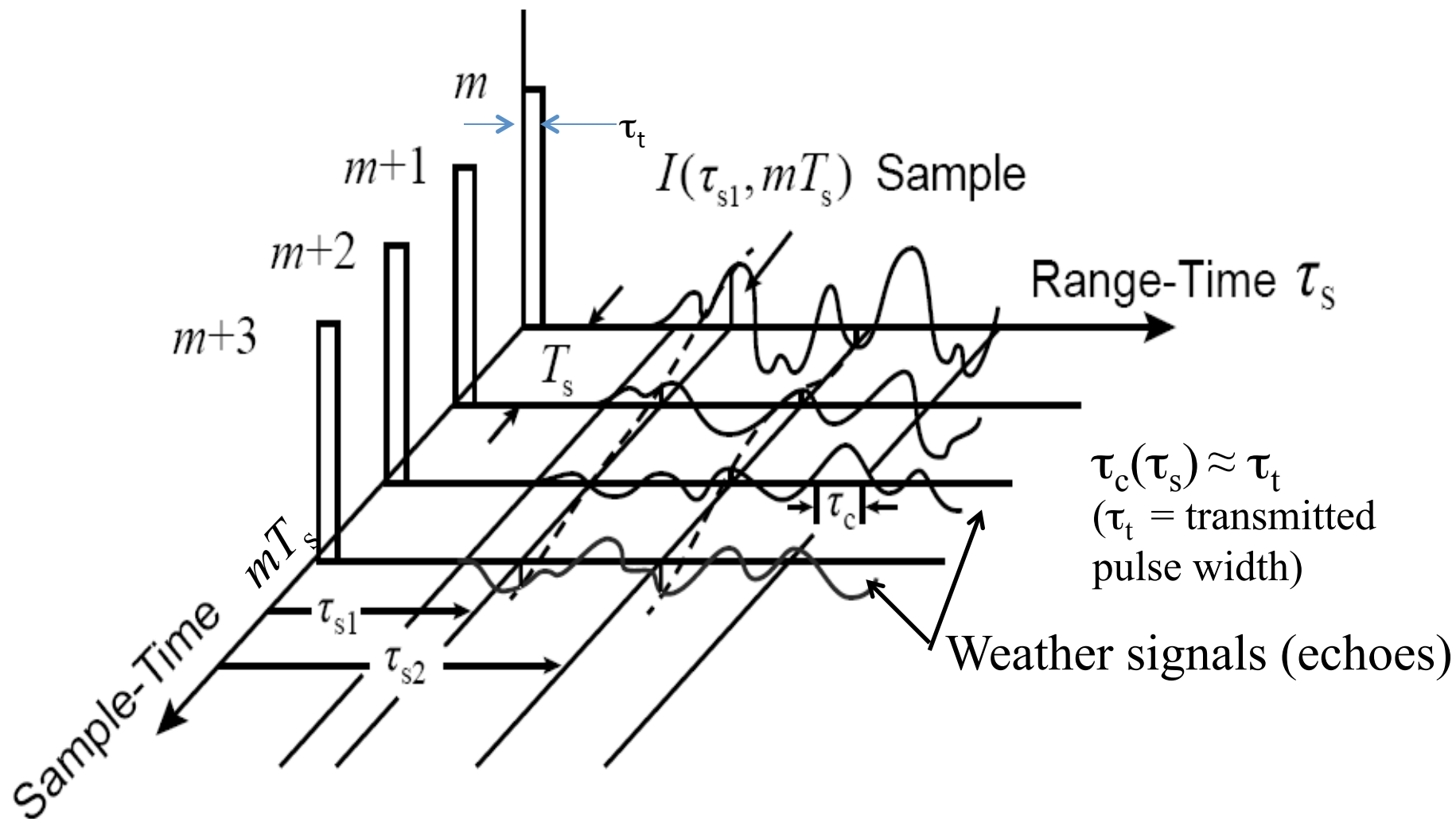
– This is a more basic constraint on radar parameters than the first equation above

- Then, σ_v and not v_a imposes a basic limitation on Doppler weather radars

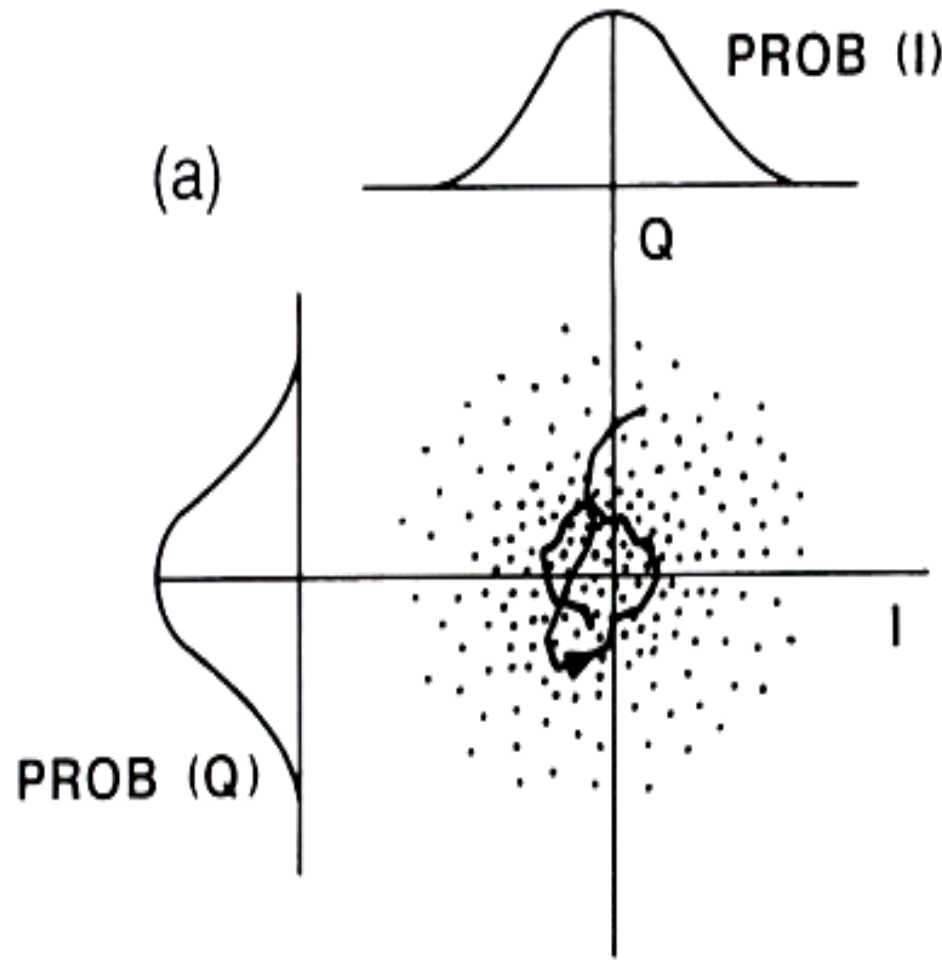
– Example: Severe storms have a median $\sigma_v \sim 4$ m/s and 10% of the time $\sigma_v > 8$ m/s. If we want accurate Doppler estimates 90% of the time with a 10-cm radar ($\lambda = 10$ cm); then, $r_a \leq 150$ km. This will often result in **range ambiguities**



Echoes (I or Q) from Distributed Scatterers (Fig. 4.1)



Weather Echo Statistics (Fig. 4.4)



RANDOM PROCESSES
 I_n AND Q_n ARE
CORRELATED

**UNCORRELATED
RANDOM VARIABLES**
(Gaussian Distribution)

Reflectivity Factor Z

(Spherical scatterers; Rayleigh condition: $D \leq \lambda/16$)

$$\eta(\mathbf{r}) = \frac{\pi^5}{\lambda^4} |K_m|^2 Z(\mathbf{r}) \quad (4.31)$$

where

$$Z(\mathbf{r}) \equiv \frac{1}{\Delta V} \sum_i D_i^6 = \int_0^\infty N(D, \mathbf{r}) D^6 dD \quad (4.32)$$

$$\eta(\mathbf{r}) = \frac{\pi^5}{\lambda^4} |K_w|^2 Z_e(\mathbf{r}) \quad (4.33)$$

for water drops : $|K_w|^2 \approx 0.93$ independent of $T(^{\circ}\text{C})$;

for ice particles : $|K_i|^2 \approx 0.16$ dependent on T and ice density.